Wear and contact fatigue properties of a novel lubricant additive

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Wet lubrication



Contact and slide





Lofrix Dry – Typhoon fighter



British Aerospace Military Aircraft & Structures Tribological and tribo-chemical test results Wear Resistance and Friction Coefficient study



-60 to 60 °C dry lubrication

1. Friction and tribofilm formation

1. Mechanical contact is necessary to form the tribofilm.



2. Behaviour of the anti-wear additives depends on the steel grade used.

1. Friction and tribofilm formation

3. Anti-wear additives form patches of the tribofilm on the surface. Scale is similar to that of the microstructure.





1. Friction and tribofilm formation



- Load
- Disc and ball speed
- Temperature

Measured:

- Tribofilm thickness vs time (interrupt test)
- Coefficient of friction vs time
- "Striebeck" curves: **COF** vs **rolling speed** (interrupt test)

In "timed step" (normal operating mode) disc moves faster than the ball. In "Striebeck step" two measurements are done; one with ball moving faster and one with disc moving faster.



Grade	С	Mn	Si	Cr	Ni	Mo	V	W	
100Cr6	0.98-1.1	0.25-0.45	0.15-0.35	1.3-1.6					
440C	0.95-1.2	1	1	16-18	≤ 0.75	≤ 0.75			
M2	0.78 - 1.05	0.15 - 0.4	0.20 - 0.45	3.75 - 4.50	0.3	4.5-5.5	1.75 - 2.20	5.5-6.75	
$16 Mn Cr 5^a$	0.14-0.19	1-1.3	0.15 - 0.4	0.8-1.1				Structure	Name
^a Bulk con	nposition.						RC	$\begin{array}{c} S \\ \\ P \\ \\ P \\ \\ OR \end{array} SR$	Dithiophosphate (DTP)
							$\begin{array}{c} S \\ \parallel \\ P \\ \downarrow \\ OR \end{array} O^{-} + H_3 N^{2} \\ \downarrow \\ OR \end{array}$		R Amine thiophosphate (ATP)
							PIB O H		≻ ^{NH} ² Succinimide
							RSS		Thiadiazole
							RO	S Zn S P	Zinc dialkyl dithiophosphate (ZDDP)



Tribofilm-microstructure correlation (**M2/ZDDP**-large residual carbides)



Tribofilm-microstructure correlation (M2/ZDDP-large residual carbides)



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Jelitay Rydel et al. Tribology International 98 (2016) 74-81; 113 (2017) 13-25

Tribofilm-microstructure correlation (16MnCr5/ZDDP)



Tribofilm-microstructure correlation (**16MnCr5/ZDDP**)



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What is the tribofilm structure in dry lubricants?

Can pressure be avoided?

Is a wet lubricant required?

3. Anti-wear capabilities – roller -& spindle / shaft & break



Figure 2 Roller clamped to arm



Figure 3 Roller and spindle in contact



Figure 4 Pressure applied via a lever



Courtesy: Professor Andrew Ball, University of Huddresfield

3. Anti-wear capabilities – roller -& spindle / shaft & break



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3. Anti-wear capabilities – roller -& spindle / shaft & break



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4. Tribofilm adhesion – cutting tools



DMG Mori NVX5080

Kistler Dyno Type 9255C



2off Nikken-NBT40-C20-70 tool holders with (OSG) cutter

Steve Townley, Advanced Manufacturing and Research Centre, University of Sheffield





4. Tribofilm adhesion – cutting tools

Steve Townley, Advanced Manufacturing and Research Centre, University of Sheffield

4. Tribofilm adhesion – cutting tools Cutter wear cuts 1-30



Uncoated cutter displaying 0,21mm wear on flutes after 30 cuts

Steve Townley, Advanced Manufacturing and Research Centre, University of Sheffield

5. Evolution of coefficient of friction – rails steels



5. Evolution of coefficient of friction – rails steels



5. Evolution of coefficient of friction – rails steels



6. Nature of tribolayer – chemistry

Three classes of ashless antiwear additives studied R groups were also varied





6. Nature of tribolayer – Lofrix chemistry



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7. Nature of tribolayer – physical properties





Courtesy: Zhang et al. Tribology International 173 (2022) 107637

7. Nature of tribolayer – physical properties



8. Statistical tests and future work







8. Statistical tests and future work

- 1. Focused ion beam and production of lamellae
- 2. TEM observation of tribofilm
- 3. Characterisation of friction compounds
- 4. Comparison with Pourbaix diagrams (Thermocalc)
- 5. Comparison with literature reports

Contact

http://www.lofrix.com/products/lofrix-dry.html

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Thank you!